Amendments to the Specification

Please replace the paragraph beginning at page 17, line 1 through page 17, line 31 with the following rewritten paragraph:

In addition, the anti-slip stud 20 comprises a separate hard cermet piece 27 that extends from said outer head 31 to at least the length L_Y of the top bowl 21 and has a non-round cross-sectional shape in a plane perpendicular to the stud center line 30. According to a first alternative, said non-round cross-sectional shape of the hard cermet piece 27 is essentially a triangle or a quadrangle or a pentagon or a hexagon, having a longest diameter D3 and is located in the anti-slip stud 20, with respect to the triangular or quadrangular or pentagonal or hexagonal shape of the bottom flange 22, either essentially in the same position, in the way illustrated in figures 7 – 8, or as rotated for the degree of the toe-out angle K, in the way illustrated in figures 9 – 10. In this toe-out case, one of the longest diameters of said polygonal shape thus forms the toe-out angle, when one of the longer distances R2 or two longest distances of the bottom flange 22 are parallel with the longest diameter D1, such as the diagonal, formed by them together. Said non-round cross-sectional shape of the hard cermet piece 27 is, according to the second alternative, essentially elongate, in which case it can also be – in a way defined above – a triangle or a quadrangle or a pentagon or a hexagon, having a largest width D3 and being located in the anti-slip stud 20, so that the largest width D3 is, with respect to the longest distance R2 of the bottom flange, or respectively to the largest diameter D1, which normally is doubled with respect to the longer distance R2, either perpendicular or rotated for the degree of the toe-out angle K. Said longer distance R2 of the anti-slip stud bottom flange 22 extends to outside the envelope curve E, drawn around the jaw fingers 3, 4, 5, 6, but not more than for the distance of the second tolerance T2, in a situation where the anti-slip stud is positioned in the mutual interval 17 of the jaw fingers, as is seen in figure 14, which provides for a flexible insertion of the anti-slip stud in the stud recess together with the bottom flange bevel 25. The hard cermet piece 27 is composed of any sufficiently hard and otherwise appropriate material, known or new, generally sintered material, such as metal carbides, metal nitrides, metal oxides *etc.* On the other hand, the stud body, comprising the bottom flange 22, the top bowl and the neck portion 23, can be made, in a prior art method or in a new method, of some suitable metal alloy, such as a steel or an aluminum, or it can be made of a plastic or of a composite material. The invention neither

relates to the material of the hard cermet piece as such, nor to the material of the body as such, and therefore they are not described in more detail here, and the above mentioned materials shall be understood as examples only.

Please replace the paragraph beginning at page 20, line 3 through page 21, line 4 with the following rewritten paragraph:

The above described arrangement according to the invention is particularly well suited for the installation of studs that can be orientated and in the installation of anti-slip studs that can be orientated. In the first alternative, there are used anti-slip studs 20 provided with a non-round hard cermet piece 27 that on the cross-sectional surface is perpendicular to the stud center line 30, so that the shape of said hard cermet piece is in a constant position with respect to the shape of the bottom flange 22, *i.e.* that in every used stud 20, the longest diameter D3 or largest width D3 of the hard cermet piece 27 is located in the same predetermined position in relation to the longest diameter D1 of the bottom flange, as is seen in figures 5 – 8 and 11 – 13. Normally the largest diameter and width D3 is either perpendicular to or parallel with the largest diameter D1 of the bottom flange. In order to install such anti-slip studs in an orientating way, at least the jaw fingers 3, 4, 5, 6 of the installation tool 1 are rotated around their jaw center lines 10 for the measure of the toe-out angle K, as marked by dotted lines in figure 15 and in figures 1A and 3A in relation to figure 2. Now the installed anti-slip studs 20 are in such a position, in which they are as turned around their stud center lines 30 for the measure of the toe-out angle K, because the jaw fingers force the bottom flange 22 to turn along for the same toe-out angle, so that the hard cermet pieces 27 are orientated in the tire in a predetermined position with respect to said rotation axis line P2. Secondly, in said alternative there are used such mutually different anti-slip studs 20 of which in the first type of studs the shape of the hard cermet piece is as turned for the measure of the toe-out angle K in relation to the shape of the bottom flange 22, and of which in the second type of studs said toe-out angle does not exist. In the first type of anti-slip studs 20, the longest diameter D3 or largest width D3 of the hard cermet piece 27 is typically located either in parallel with or perpendicular to the longest diameter D1 of the bottom flange, as is seen in figures 2 and 5 – 8, as well as 11 – 13, and in the second type of anti-slip studs 20, the longest diameter D3 or largest width D3 of the hard cermet piece 27 is located as turned for the measure of the toe-out angle K in relation to the longest diameter D1 of the bottom flange or in relation to

a line perpendicular to the longest diameter D1, as is seen in figures 1B and 3B, as well as 9 - 10. Now at least the mutual positions of the jaw fingers 3, 4, 5, 6 of the installation tool 1 are maintained, in directions perpendicular to the jaw center line 10, in a constant position with respect to the rotation axis line P2, but the first type of anti-slip studs to be installed are replaced by the second type of anti-slip studs or vice versa, *i.e.*, the type of the anti-slip studs to be installed is changed in order to orientate the studs in a predetermined position with respect to said rotation axis line P2.